

**A STUDY OF BASE TRANSIT TIME AND GAIN OF INP-INGAAS HBTs FOR UNIFORM AND NEARLY GAUSSIAN BASE DOPING PROFILES****Prasenjit Saha and Sukla Basu**

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Received 22-08-2012, revised 09-09-2012, online 12-09-2012

**ABSTRACT**

A detailed study on InP-InGaAs Heterojunction Bipolar Transistor is presented in this paper. Two important factors for determining the performance of a transistor are base transit time ( $\tau_b$ ) and current gain ( $\beta$ ). Variations of base transit time and gain with temperature and other device parameters for both uniform and non uniform base doping profiles are studied here. Dependence of diffusion constant on temperature and doping concentration are taken into account in this study.

**Keywords:** InP/InGaAsHBT, Base Transit time; Current Gain.

**I. INTRODUCTION**

Heterojunction bipolar transistors (HBTs) using III-V compounds are of great importance in high frequency and power applications. Among these HBTs GaAs based systems are much studied in literature[1],[2],[3]. InP based technology has numerous advantages over GaAs technologies for many applications and the rapidly expanding demand for broadband telecommunications provides a strong market pull for the enabling performance. Recently, remarkable advances of InP-InGaAs HBTs and InGaAs based HEMTs have been achieved [4],[5],[6],[7] and they have become important due to their excellent current handling capability, superior frequency performance (provided by InP microelectronics) and high speed performance, which is obtained due to high electron mobility in the p type InGaAs base region. Further improvement in speed performance of these devices can be obtained by reducing base resistance which requires high doping concentration. On the other hand low doping concentration reduces junction capacitance and tunneling leakage current of either the BE or CB junction. The doping profile (nearly Gaussian) considered here meets both of these requirements. Moreover linear grading of the In content across the base can create a built-in field which can further decrease  $\tau_b$ . Again mobility of carrier is another important factor on which both transit time and current gain are dependent. Mobility of carriers through base depends on temperature as well as on doping concentration and composition of base. In the present paper, effect of base doping profile and composition of base material on base transit time and gain is analyzed including the effect of temperature variation.

**II. THEORY**

Base transit time of InP/InGaAs HBTs by Kroemer's double integration formula is given by [8]

$$\tau_b = \int_0^{W_b} \frac{n_i^2(x)}{N_a(x)} \left[ \int_x^{W_b} \frac{N_a(y)}{D_n n_i^2(y)} dy + \frac{N_a(W_b)}{V_{sat} n_i^2(W_b)} \right] dx \quad (1)$$

where  $W_b$  is the neutral base width,  $N_a$  is the p type base doping concentration,  $D_n$  is the electron diffusion coefficient in the InGaAs base,  $n_i$  is the intrinsic carrier concentration of the InGaAs base and  $V_{sat}$  is the saturation velocity of minority carrier in base. Ballistic transport of carriers is not considered in (1) since clear ballistic behavior is observed only when base width is a small fraction of mean free path of carriers[9].

Assuming Einstein's relation holds good

$$D_n = \frac{kT}{q} \mu_{n(\text{InGaAs})} \quad (2)$$

where  $\mu_{n(\text{InGaAs})}$  is the electron mobility in the InGaAs base,  $k$  Boltzmann constant,  $T$  absolute temperature and  $q$  electronic charge. Mobility in InGaAs is related to mole fraction of In by the relation [10]

$$\mu_{n(\text{InGaAs})} = y_t \mu_{n(\text{InAs})} + (1-y_t) \mu_{n(\text{GaAs})} \quad (3)$$

where,  $y_t$  is the total In content in the base,  $\mu_{n(\text{InAs})}$  is the electron mobility in InAs,  $\mu_{n(\text{GaAs})}$  is the electron mobility in GaAs. Here the values of  $\mu_{n(\text{InAs})}$  and  $\mu_{n(\text{GaAs})}$  are considered as 22600 cm<sup>2</sup>/v-s and 8500 cm<sup>2</sup>/v-s respectively [11].

Mobility is dependent on temperature ( $T$ ) as well as on doping concentration and is given by the relation [12]

$$\mu = \mu_{min} + \frac{\mu_{max(300K)} (300/T)^{\theta_1} - \mu_{min}}{1 + \left( \frac{N_a}{1.3 \times 10^{17} \times (T/300K)^{\theta_2}} \right)^\lambda} \quad (4)$$

For InGaAs  $\mu_{min}$  and  $\mu_{max(300K)}$  are 300 cm<sup>2</sup>/v-s and 14000 cm<sup>2</sup>/v-s respectively.  $N_{ref}$  at 300K is  $1.3 \times 10^{17}$  cm<sup>-3</sup>.  $\theta_1=1.59$ ,  $\theta_2=3.68$ ,  $\lambda=0.48$  [12].

Using these values mentioned above mobility in InGaAs can be found.

Current Gain of InP/InGaAs HBT is given by [13]

$$\beta = \frac{v_B}{W_b f_R \left[ 1 + \left( \frac{v_B}{V_{sat}} \right) \right]} = \frac{1}{f_R \left[ \left( \frac{W_b^2}{2D_n} \right) + \left( \frac{W_b}{V_{sat}} \right) \right]} \quad (5)$$

where,  $v_B$  is effective electron velocity through the neutral base region,  $f_R$  is recombination factor.  $f_R$  is given by [13]

$$f_R = C_{AP}N_a^2 + (C_{BB} + C_{SRH})N_a \quad (6)$$

where,  $C_{AP}$  is Auger coefficient for holes,  $C_{BB}$  is band-to-band radiative coefficient;  $C_{SRH}$  is Shockley-Read-Hall coefficient. Here  $f_R$  is calculated as  $1.6 \times 10^9 \text{ s}^{-1}$  [13] considering  $N_a$  as  $10^{19} \text{ cm}^{-3}$ , base width ( $W_b$ ) is taken as 50nm and  $V_{sat}$  is taken as  $8 \times 10^6 \text{ cm/s}$  [15].

From (1) base transit time for uniform base doping profile can be written as

$$\tau_b = W_b^2/2 D_{n(\text{InGaAs})} \quad (7)$$

**II.1. Base transit time and gain for nonuniform base doping profiles without considering variation of electron diffusion constant with doping concentration**

Following base doping profile (fig: 1) is considered here [14].

$$N_a(x) = N_p \sin\left(\frac{(3.12-\alpha)x}{W_b} + \alpha\right) \quad (8)$$

where  $0 \leq x \leq W_b$  and  $\alpha$  varies from 0.1 to 1.57 and  $\alpha = \sin^{-1} \frac{N_0}{N_p}$ .

No is the doping concentration near the emitter,  $N_p$  the peak concentration in the base,  $W_b$  the base width. At the base-emitter junction (i.e. at  $x=0$ ),  $N_0 = N_p \sin(\alpha)$  and at the base-collector junction (i.e. at  $x=W_b$ ) the doping concentration is  $N_p \sin(3.12) = 0.22N_p$ .

By using (1) the base transit time for the profile in(8) can be written as

$$\tau_b = \frac{-1.998 W_b^2 \log\left(\sin\frac{\alpha}{2}\right)}{D_n(3.12-\alpha)^2} + \frac{0.043 W_b}{V_{sat}(3.12-\alpha)} + \frac{-0.022 W_b \left(\log\left(\tan\frac{\alpha}{2}\right)\right)}{V_{sat}(3.12-\alpha)} \quad (9)$$

The first term inside the bracket of (5) represents base transit time for uniform profile. The current gain of Inp-InGaAs HBT for non uniform base doping profile of (8) can be calculated from equation (5) by replacing the first term inside the bracket by the expression for transit time ( $\tau_b$ ) obtained in (9).

**II. 2. Transit time and Gain for non uniform base doping profile taking electron diffusion coefficient as function of base doping concentration and temperature**

Here diffusion coefficient is function of base doping concentration and temperature. So, diffusion coefficient is included in the integration. The transit time is calculated using (1) as,

$$\tau_b = \int_0^{W_b} \frac{n_i^2(x)}{N_a(x)} \left( \int_x^{W_b} \frac{N_a(y) dy}{D_n(N_a(x)) n_i^2(y)} \right) dx + \int_0^{W_b} \frac{n_i^2(x) N_a(W_b) dx}{N_a(x) V_{sat} n_i^2(W_b)}$$

$$= \int_0^{W_b} \frac{1}{N_a(x)} \left( \int_x^{W_b} \frac{N_a(y) dy}{D_n(N_a(x))} \right) dx + \int_0^{W_b} \frac{N_a(W_b) dx}{N_a(x) V_{sat}} \quad (10)$$

where  $\mu_n$  and  $D_n$  are functions of  $N_a(x)$  and T. By using (4) and the values of  $\mu_{min}, \mu_{max}(300K), \theta_1$  for InGaAs we obtain:

$$\mu_{\text{InGaAs}} = 300 + \frac{\left(\frac{121549400}{T^{1.59}} - 300\right)(6763.8T^{1.77})}{6763.8T^{1.77} + N_a(x)^{0.48}} \quad (11)$$

Now, for the ease of calculation some replacements are made like 300 as A,  $\left(\frac{121549400}{T^{1.59}} - 300\right)(6763.8T^{1.77})$  as B and  $6763.8T^{1.77}$  as C.

Then Eq. (11) can be written as

$$\mu_n(N_a(x)) = A + \frac{B}{C + N_a(x)^{0.48}} \quad (12)$$

Diffusion coefficient can be written using (12) as

$$D_n(N_a(x)) = \frac{kT}{q} \mu_n(N_a(x)) \quad (13)$$

where base doping profile is taken as (8). Here for the purpose of simplification, the term  $B + A(C + N_a(y)^{0.48})$  is replaced by  $8.2A(C + N_a(y)^{0.48})$  in the calculation of  $\tau_b$  in equation (10). The average value of the above terms are nearly equal. After the calculation A, B, C were replaced by their original values.

Now from (8),(10) and (13) we get,

$$\tau_b = \frac{W_b^2 \left(\log\left(\sec^2\frac{\alpha}{2}\right)\right)}{0.2137(3.12-\alpha)^2} + \frac{0.02 W_b (1.97 - \log\left(\tan\frac{\alpha}{2}\right))}{V_{sat}(3.12-\alpha)} \quad (14)$$

and Gain is calculated from (5).

**II.3. Base transit time and gain for the non uniform base doping profile and linear grading of composition.**

Intrinsic carrier concentration of InGaAs base is written as

$$n_i^2(\text{InGaAs}) = N_c N_v \exp\left[\frac{-E_g(\text{InGaAs})}{kT}\right] \quad (15)$$

where  $N_c, N_v$  are the effective density of states in the conduction band and valance band respectively,  $E_g(\text{InGaAs})$  is the energy gap of InGaAs base which is in the form  $E_g(\text{InGaAs}) = y_t E_g(\text{InAs}) + (1-y_t) E_g(\text{GaAs})$ , and  $E_g$  of InGaAs is given by [10].

Using linear variation of composition:

$$E_g(\text{InGaAs}) = -A x + B \tag{16}$$

where  $A = [1.07x(y_{tc} - y_{te})/W_b]$  and  $B = [1.43 - (y_{te} \times 1.07)]$ ,  $y_{te}$  and  $y_{tc}$  are the mole fractions of In at the emitter end of the base and the collector end of the base respectively.

$$n_{i(\text{InGaAs})}^2 = N_c N_v \exp\left[\left(\frac{A}{KT}\right) x - \left(\frac{B}{KT}\right)\right] \tag{17}$$

Using (1) base transit time for the profile in (8) can be written as

$$\tau_b = a + b + c \tag{18}$$

$$\text{where } a = \frac{0.11 W_b^2 \left(\frac{AW_b}{KT} - 0.7\right)}{D_n \left(1 + \frac{A^2 W_b^2 0.11}{(KT)^2}\right)}$$

$$b = -\left(\frac{0.33 W_b \left(0.01 \frac{AW_b}{KT} - 1\right) \left(46.3 - 10 \exp\left(-\frac{AW_b}{KT}\right)\right)}{AD_n \left(1 + \frac{0.11 A^2 W_b^2}{(KT)^2}\right)}\right) \text{ and}$$

$$c = \frac{(0.9 - 0.2 \exp\left(-\frac{AW_b}{KT}\right))}{\frac{AV_{sat}}{KT}} \text{ and here the composition}$$

variation the electron diffusion coefficient has been taken as independent of composition variation; the expression of  $n_{i(\text{InGaAs})}^2$  in (17) is substituted in (1) to find the transit time.

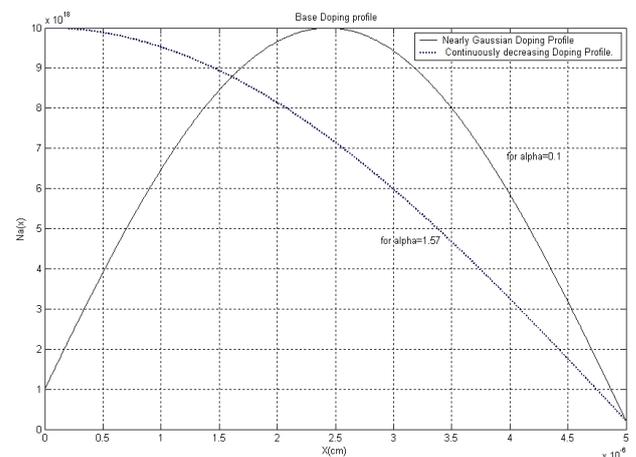
Here  $KT = 26 \text{ meV} = 0.026 \text{ eV}$ ,  $A = [1.07 \times \frac{(y_{tc} - y_{te})}{W_b}]$  and  $\text{delz}$  is taken as  $(y_{tc} - y_{te})$  and the gain can be calculated by (5).

### III. RESULTS AND DISCUSSION

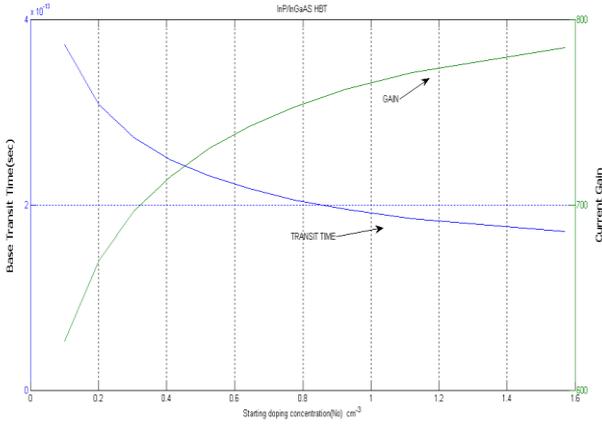
In Fig. 1, the non uniform base doping profile of InP-InGaAs has been shown, which is nearly Gaussian in nature when  $\alpha$  is taken as 0.1 and  $N_p = 10^{19} \text{ cm}^{-3}$ . When  $\alpha$  is taken as 1.57 the starting doping concentration is the peak concentration which occurs at the base-emitter junction.

In Fig. 2, using the base doping profile in (8) and with the help of (1), (5), (9) base transit time and gain are calculated and plotted against the fraction ( $\alpha$ ) which indicates the pattern of the base doping profile. It shows that transit time decreases and gain increases with the

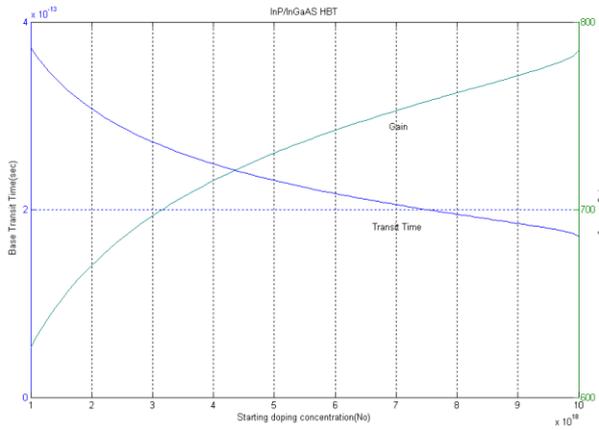
increase of  $\alpha$ . Fig. 3 shows that as the doping concentration near emitter ( $N_0$ ) increases the base transit time decreases and gain increases. Fig. 4 shows that as the base width ( $W_b$ ) increases, the base transit time increases and the gain decreases. Using (5) and (9) the gain and transit time are calculated. Figure 5 shows that transit time decreases and gain increases with an increase in temperature from 250K to 350K. In Fig. 6, using the base doping profile in (8) and with the help of (1), (5), (11), the base transit time and gain are calculated and plotted against the base width. Here with the increase of base width the gain decreases and the transit time increases. In Fig. 7, the effect of In mole fraction grading on  $\tau_b$  and  $\beta$  is shown. Here the In grading is varied from 0%-10% ( $\text{delz} = 0.1$ ) to 0%-30% ( $\text{delz} = 0.30$ ). As the gradient of mole fraction of In in the base increases the base transit time decreases and the gain increases. Fig. 8 and Fig. 9 show the comparison of gain and transit time's dependence on temperature for uniform and non uniform base doping profile. It is easily seen that the gain curve of non uniform doping profile is located higher in the gain axis than the curve for the uniform doping profile and transit time curve of non uniform doping profile is located lower in the transit time axis than the curve for the uniform doping profile. The temperature has not much effect the transit time of a non uniform doping profile.



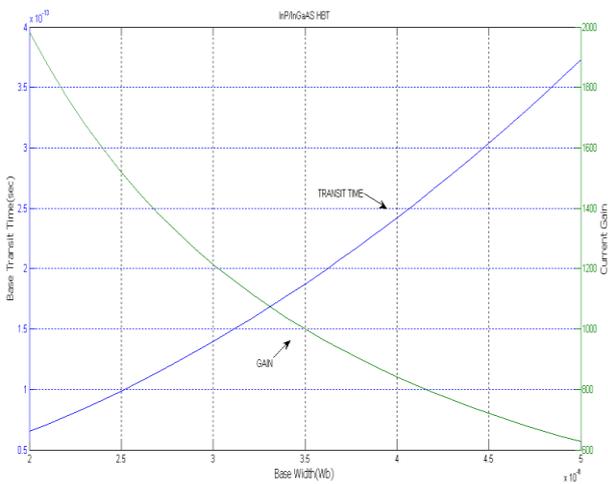
**Fig. 1:** Nearly gaussian base doping profile ( $\alpha=0.1$ ) and continuously decreasing doping profile for  $\alpha=1.57$ .



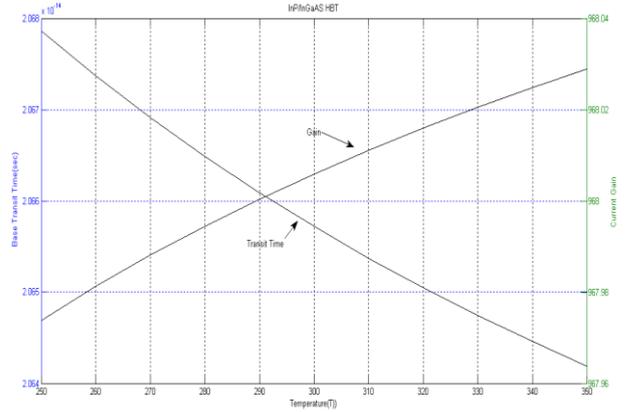
**Fig. 2:** Transit time /gain vs profile fraction ( $\alpha$ ).  $D_n=415$  cm<sup>2</sup>/s,  $y_t=0.53$ .



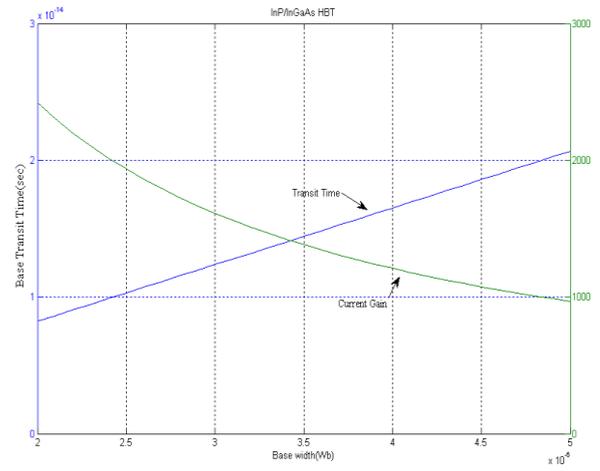
**Fig. 3:** Transit time /gain vs starting doping concentration ( $N_0$ ),  $D_n=415$  cm<sup>2</sup>/s,  $y_t=0.53$ .



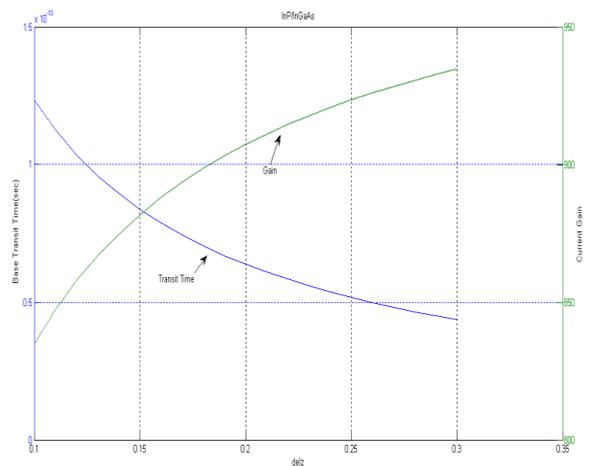
**Fig. 4:** Transit time /gain vs base width,  $D_n=415$  cm<sup>2</sup>/s,  $y_t=0.53$ .



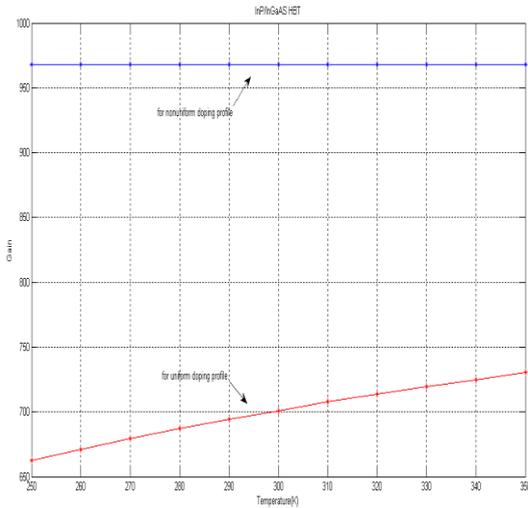
**Fig. 5:** Transit time /gain vs temperature. Diffusion coefficient is function of doping concentration and temperature.



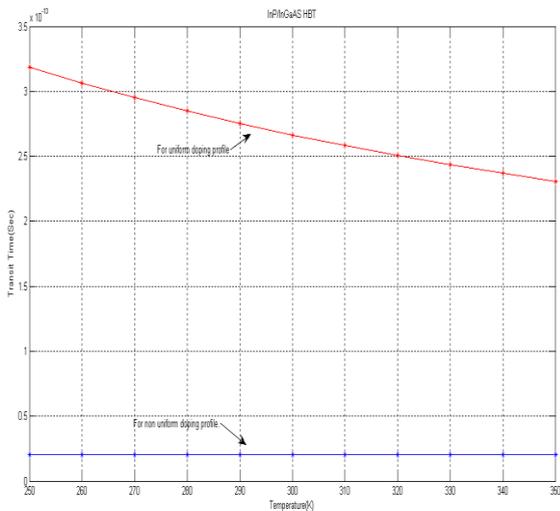
**Fig. 6:** Transit time /gain vs base width. Diffusion coefficient is function of base doping concentration .i.e function of  $x$  and temperature,  $T=300$ K.



**Fig. 7:** Transit time /gain vs  $\delta z$ ,  $D_n=415$  cm<sup>2</sup>/s,  $y_t=0.53$ .



**Fig. 8:** comparison between gain vs temperature plot for uniform and non uniform nearly Gaussian doping profile.



**Fig.9:** Comparison between transit time vs temperature plot for uniform and non uniform nearly Gaussian doping profile.

**IV. CONCLUSION**

Results obtained from the analytical model of the InP/InGaAs HBT shows that higher current gain can be achieved from nonuniform base doping profile (here which is nearly Gaussian in nature) than the uniform base doping profile. High Temperature and low doping concentration ( $N_b$ ) give low base transit time. It is found that rate of decrease of  $\tau_b$  and rate of increase of  $\beta$  become lower as  $N_b$  approaches  $N_p$ . The  $\tau_b$  increases

considerably and gain decreases with the increases in base width ( $W_b$ ). But  $\tau_b$  decreases considerably and gain increases with the increases in gradient of mole fraction of In (Indium) in the base. When diffusion coefficient is function of doping concentration and temperature then their contribution is taken into account for the calculation. Moreover when the profile has the highest concentration at the base-emitter junction ( $\alpha= 1.57$ ), the gain is more than when the profile has the peak value at the middle of the base ( $\alpha= 0.1$ ). But, in order to reduce junction capacitance and tunneling leakage current of the base emitter junction, doping concentration should be low at both the junctions. The base doping profile which has been taken here (Nearly Gaussian,  $\alpha= 0.1$ ), gives the optimum base transit time and moderate current gain.

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